



NATIONAL ENERGY TECHNOLOGY LABORATORY



Database and Model of Coal-fired Power Plants in the United States for Examination of the Costs of Retrofitting with CO₂ Capture Technology

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EXECUTIVE SUMMARY

Given the importance of coal to power generation in the United States, where coal-fired power plants supply around 50 percent of the Nation's electricity needs, examination of the costs and practicability for retrofit of existing pulverized coal power plants with CO₂ capture technology is a valid exercise. To help elucidate this issue, this study defines a viable population of pulverized coal plants, which were examined individually to determine costs and space availability for retrofit. The task was to assess coal-fired power plants in the U.S. relative to the cost and feasibility for retrofitting with CO₂ capture technology.

The effort comprised the development of a database and geographic information systems (GIS) modeling analysis of coal-fired power plants in the U.S. to conduct the assessment. The viable population for the analysis was defined as those active plants with a combined unit generation capacity greater than 100 MW, an average heatrate below 12,500 Btu/kWh, and a location within 25 miles of a potential carbon sequestration opportunity. The resultant population totals 324 plants. Of these, 290 had the requisite data to complete the analyses, comprising 275 GW. The plants were then evaluated individually.

The analysis is based upon the NETL 2007 publication *Carbon Dioxide Capture from Existing Coal-Fired Power Plants* (Conesville study) as a foundation for the application of carbon capture retrofit technology in terms of cost and layout. Central to the analysis is the quantitative GIS model, entitled the Carbon Capture Model (CCM). The CCM comprises programmatically linked databases, GIS map documents, and report spreadsheets that calculate capital expense (CAPEX), operating expense (OPEX), and parasitic load associated with retrofitted carbon capture technology. The model evaluates these parameters by scaling costs using the plant-specific parameters and algorithms derived based upon the Conesville study. A GIS imagery analysis of each plant was conducted to modify construction costs due to specific site requirements by assigning construction difficulty factors to retrofit components. Cost-supply curves relative to the viable population were developed.

Results of the analysis indicate that, for the 50th percentile (142 GW) of the analyzed viable population, the CO₂ capture total cost (calibrated to the Conesville study) would be about \$61/tonne or less. To retrofit 90 percent of generation capacity (about 254 GW), the total capture cost would be about \$80 per tonne or less. It should be noted that this study provides an overview of the plant sites. It is not an engineering-level analysis of individual plants and does not address the consequences of design.

1.0 Introduction

The effort comprised the development of a database and geographic information systems (GIS) analysis of a defined population of coal-fired power plants in the U.S. to model the cost and assist in the assessment of the feasibility of retrofitting these plants with CO₂ capture technology. This report covers data sources, methodology employed, modeling and results.

2.0 Methodology

Fundamentally, this effort is based upon the NETL 2007 publication *Carbon Dioxide Capture from Existing Coal-Fired Power Plants* (Conesville study) as a foundation for the application of carbon capture retrofit technology in terms of cost and layout.

As a central part of the database and analysis effort, the CCM comprises programmatically linked databases, GIS map documents, and report spreadsheets that calculate capital expense (CAPEX), operating expense (OPEX), and parasitic load associated with retro-fitted carbon capture technology.

In addition to the Conesville Study, additional references for cost and other information include:

- *Cost and Performance Baseline for Fossil Energy Plants*, (“Baseline Report”), DOE/NETL-2007/1281, Volume 1: Bituminous Coal and Natural Gas to Electricity, Final Report, Revision 1, August 2007
- *Pulverized Coal Oxycombustion Power Plants* (Oxycombustion Report), NETL, Final Results, August 2007
- *Reduced Water Impacts Resulting from Deployment of Advanced Coal Power Technologies*, (Water Report) NETL, Chris Nichols and Phil DiPietro, December 16, 2007

The primary source of data on physical plant parameters such as unit nameplate capacity, heat-rate, and emissions was Ventyx Corporation’s Energy Velocity (EV) Suite, a compilation of energy industry and market databases.

2.1 Viable Population

The viable population for the study was initially defined to be operating U.S. coal-fired power plants greater than or equal to 100 MW total nameplate capacity with a weighted average heat-rate equal to or less than 12,500 Btu/kWh. This definition was refined to include a distance to sequestration opportunity criterion.

A GIS analysis of each power plant’s proximity to each of three sequestration opportunities: oil and gas fields, saline aquifers, and existing CO₂ pipelines was performed. The results show that a total of 324 (83.5%) plants of the viable population are within 25 miles of a sequestration opportunity.

Therefore, a 25 mile distance was used to represent a reasonable threshold for a viable transportation of CO₂ within the CCM. This is more conservative than NETL's Bituminous Baseline Final Report¹, where 50 miles was used as an appropriate distance for CO₂ transportation to a saline aquifer.

With the addition of distance to the sequestration criterion, the viable population consists of 324 plants. Of these 324 plants, suitable imagery was not available for three, and EV emissions data required for analysis was missing from 31, resulting in a final population of 290 plants that meet selection criteria and data requirements.

2.2 Model Development and Analysis

The CCM was developed to merge and analyze the various disparate datasets. It functions by reading parameters from the EV datasets and GIS data sources for the population of plants. The model then calculates the required size and cost for the various CO₂ capture components using the Conesville study to determine scaling functionality. Costs are adjusted for construction difficulty, water availability, and additional land requirements. Further detail on the derivation of specific parameters is presented below.

The CCM is based upon the Conesville study, which examined the cost and physical footprint requirements of retrofitting the 463.5 MW AEP Conesville Unit 5 with amine-absorber carbon capture technology. Figure 1 illustrates the required equipment.

Critical to the CCM is a GIS imagery analysis that identifies construction difficulties associated with space constraints and existing plant layout. This analysis was used to modify the estimated CAPEX to account for increased cost of engineering and construction and the cost of additional land if needed.

The Conesville study examined four cases with varying effective CO₂ absorption percentages of 90, 70, 50 and 30 percent. The CCM assumes that retrofitted plants will scrub 90 percent of the emitted CO₂.

Fortunately, the Conesville study assumed use of CO₂ absorption equipment with a scrubbing capability of 90 percent—the study's various cases were achieved by limiting the amount of flue gas diverted to the CO₂ absorbers—which allowed an imputed calculation of power plant size if the equipment for each of the cases was operative at 90 percent capacity.

¹ *Cost and Performance Baseline for Fossil Energy Plants*, DOE/NETL-2007/1281, 2007

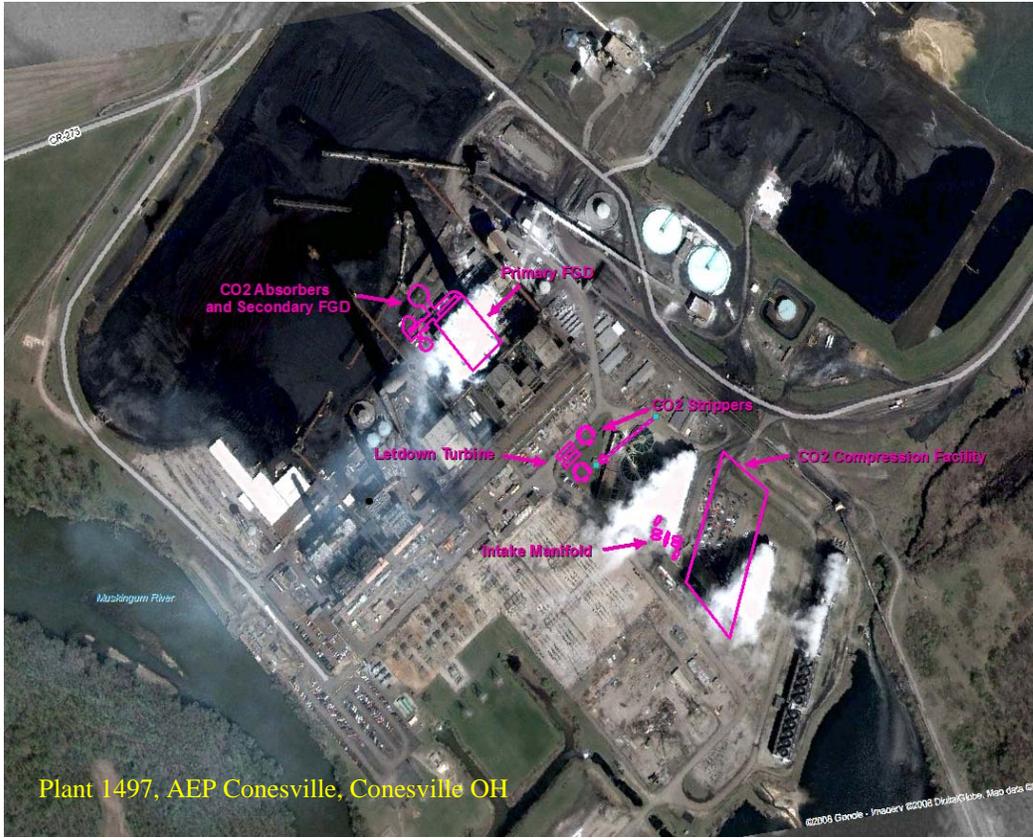


Figure 1. Retrofit equipment layout for Conesville Unit 5

Additionally, based upon the Conesville study, the cost of CO₂ scrubbers and absorbers did not vary among the scenarios. The assumption was made that these components are not sensitive to the amount of CO₂ being scrubbed and therefore not sensitive to the size of the plant. Consistent with the Conesville study for initial purposes, a cost of \$17.66 million per retrofitted unit was used in this analysis. These costs will be subject to further refinement.

Other components were found to vary in cost among the cases or were dependant upon the presence and effectiveness of current sulfur and nitrous oxide emissions control equipment.

A complete retrofit of Conesville Units 4, 5, and 6 was modeled using the Conesville study as a guide. Conesville then served as a baseline for comparison of retrofit difficulty at other plants. Figure 2 shows AEP Conesville retrofitted with carbon capture equipment on its three operating units.

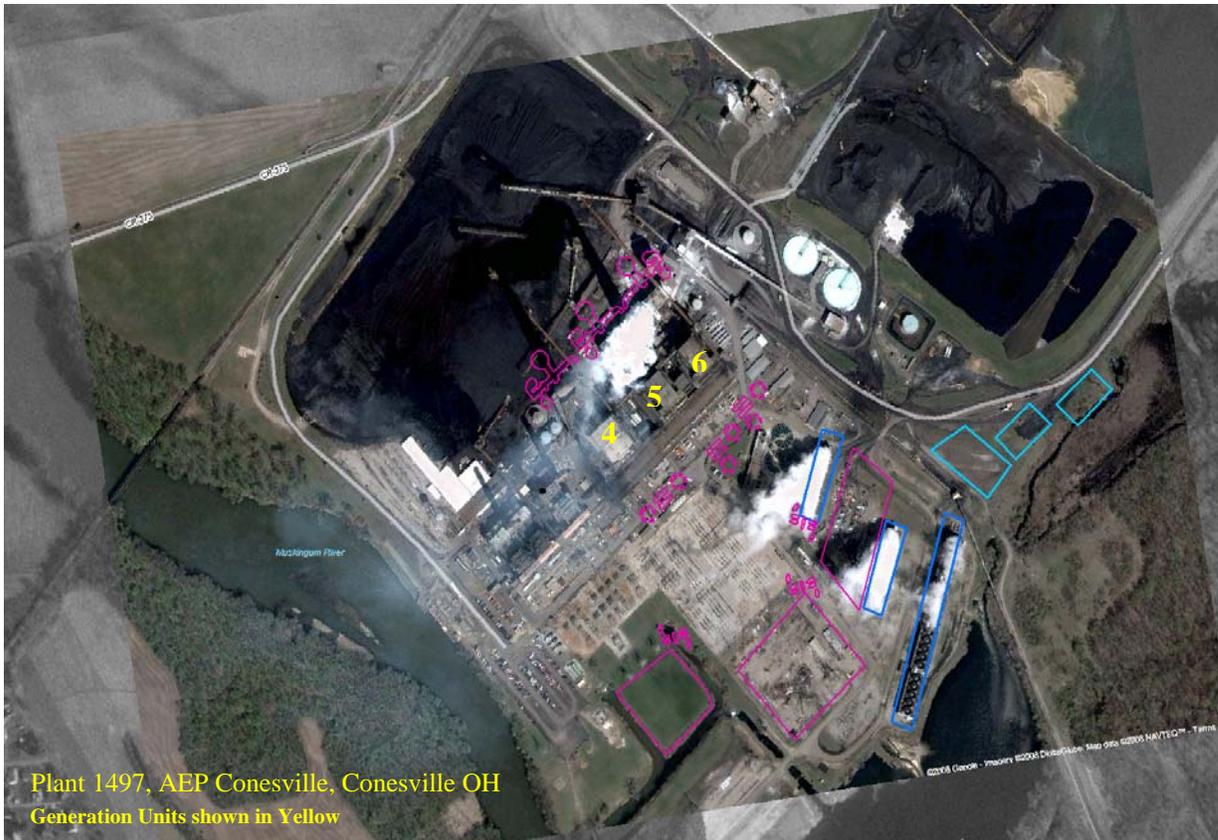


Figure 2. Complete Conesville retrofit

2.2.1 SO₂ Removal

SO₂ removal is necessary for amine-absorber carbon capture technology. Accordingly, requirements for flue gas desulfurization (FGD) were assessed for each site for sulfur removal to a level of 98 percent was assessed in terms of cost and space. For sites that have FGD that do not remove sulfur to this level, or for sites without FGD, the need for required FGD equipment was assessed. In addition, to bring sulfur levels to the maximum 10 ppm requirement of the CO₂ scrubbers, separate sulfur “polishing” was assessed. Calculations were made in the CCM as follows based upon costs found in literature:

- In plants without primary FGD systems, new construction costs of \$105.5 per kilowatt capacity for the primary FGD system designed to remove 98 percent SO₂, and a value of \$94.60/ton for the additional sulfur removed by sulfur polishing down to 10 ppm were used. An example is Conesville’s 841.5 MW Unit 3; currently without primary FGD. At a cost of \$105.5/kW, the Conesville Unit 3 FGD would cost \$88.5 million for installation of FGD.
- In plants with current primary FGD systems, the current SO₂ removal percentage was estimated using emissions and coal data from the EV datasets, the marginal SO₂ removal needed to achieve 98 percent was calculated and the marginal additional removal requirement was prorated at a cost of \$96.5 per kilowatt

capacity accordingly. The sulfur polishing cost of \$94.60/ton was then applied to the additional sulfur reduction to 10 ppm.

2.2.2 NO_x Removal

Consistent with the Oxycombustion report, and to be compliant with environmental requirements, the CCM requires NO_x emissions to be at or below 0.07 lbs NO_x/ million Btu for purposes of CO₂ capture. NO_x emissions data for each unit was compared to this target rate to determine the additional NO_x scrubbing requirement. Using the unit's total Btu value and an installation cost of \$300/tonne NO_x, a value for NO_x scrubbing cost was calculated.

2.2.3 Construction Difficulty Factors

In analyzing the sampled plant sites it became apparent that some plants are more crowded than others. Two construction cost factors were determined to accommodate this situation—a “close-in” cost of construction difficulty factor and a “landscape” cost of construction difficulty factor.

Close-in Construction. The letdown turbine, CO₂ scrubbers and absorbers, as well as the primary and secondary FGD's require construction in close proximity to the turbine and flue stack. The layout of some plants can easily accommodate these additional components. However, for plants where space is more crowded, an incremental factor was applied to account for anticipated difficulty in construction. These factors were ranged from 0 (easily constructed) to 40 percent (difficult to construct). Plants with a zero factor were determined to have a construction difficulty comparable to the Conesville baseline plant.

Landscape Construction. At the Conesville plant, as depicted in Figure 2, designs were created to individually retrofit Units 4, 5, and 6 with all required components. However, it was assumed that CO₂ compression and additional cooling facilities could be combined into larger plant (as opposed to unit) -servicing components. Note that, while some adjustments and accommodations will need to be made, there are no large structures or other significant obstacles to overcome or work around with close-in construction at the Conesville site. The CO₂ compression facility and additional cooling towers can be built in proximity to the plant, allowing more latitude for siting them. Still, these components are by far the largest and require significant open space at a plant. Similar to the Close-in factor, values ranged from 0 to 30 percent.

2.2.4 Total Investment CAPEX

In the model, Total Investment CAPEX for a plant is determined by the equation:

$$[(\text{Letdown Turbine Cost} + \text{CO}_2 \text{ Scrubber and Absorber Cost} + \text{FGD Cost} + \text{NO}_x \text{ Cost}) * (1 + \text{Close-In Construction Difficulty Factor})] * \text{Multiple Unit Discount} +$$

$(\text{CO}_2 \text{ Separation and Compression Cost} + \text{Additional Cooling Cost}) * (1 + \text{Landscape Construction Difficulty Factor}) + \text{Additional Land Cost}$

2.2.5 OPEX

In the CCM model, OPEX is calculated as the sum of Fixed (Labor) cost, Variable (chemical, waste, and maintenance) costs, and Feedstock cost. Figures 3 to 5 show these costs as a function of the generation capacity of the power plant based on the scenarios in the Conesville study.

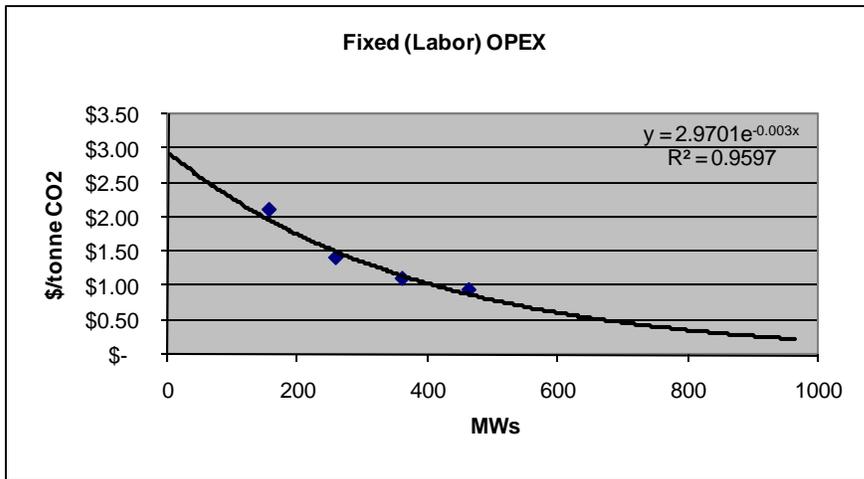


Figure 3. Fixed OPEX cost function

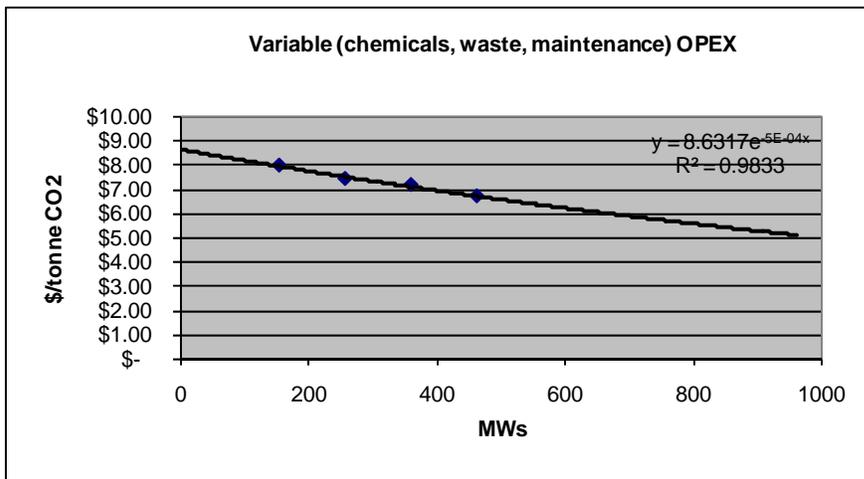


Figure 4. Variable OPEX cost function

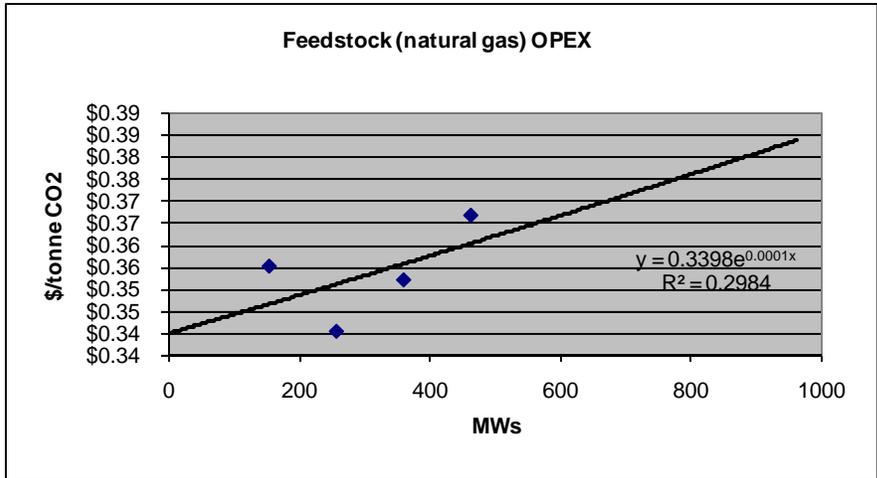


Figure 5. Feedstock OPEX cost function

2.2.6 Parasitic Load

The total parasitic load of the carbon capture retrofit is equal to the sum of the parasitic loads of the newly installed NO_x and SO₂ control equipment, the additional cooling, and the actual CO₂ retrofit components.

A parasitic loading function was developed based on Conesville study cases for the retrofit equipment. Figure 6 shows this as a function of nameplate capacity.

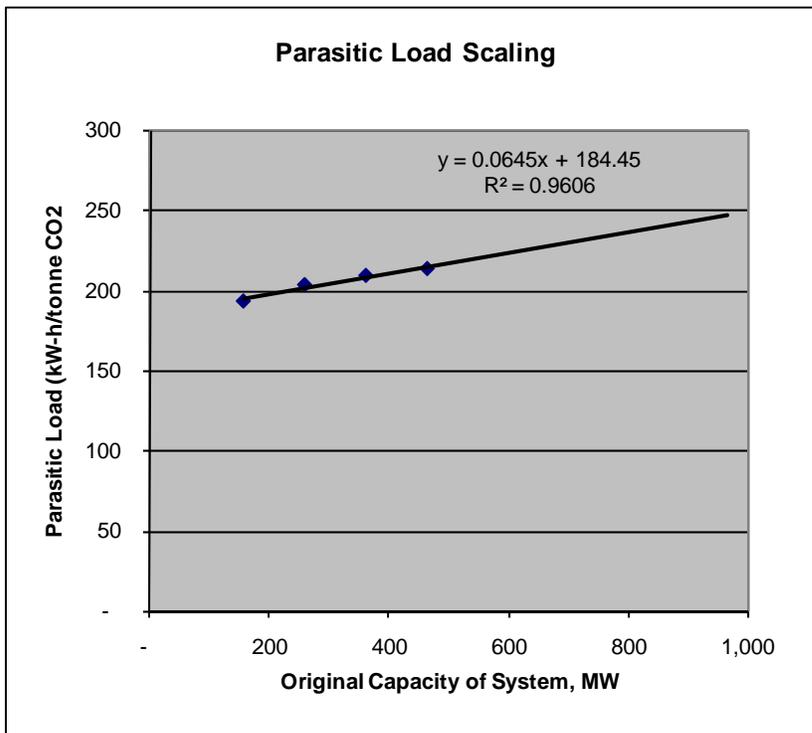


Figure 6. Parasitic load scaling for retrofit components

In addition, parasitic load factors associated with NO_x, SO₂, and additional cooling were developed based upon the Baseline report. A factor of 0.0001 kW parasitic load/kW capacity was used for NO_x equipment and a value of 0.0091 kW parasitic load/kW capacity was used for SO₂ equipment. Additional cooling was determined to have a parasitic load of 0.033 kW parasitic load/kW capacity. These four components are added and reported as total parasitic load in units of kWh/tonne CO₂-captured. Five cents per kWh was used to calculate a \$/tonne CO₂-captured parasitic load cost.

3.0 Results

This section provides the analytical results from the CCM. CAPEX, OPEX, and parasitic costs were calculated for each of the 290 plants of the viable population. Figure 7 shows cumulative nameplate capacity as a function of uncalibrated CO₂ capture CAPEX. For plants in the the 50th percentile, the capital investment cost is less than \$10/tonne.

Figure 8 shows CO₂ capture CAPEX as a function of nameplate capacity for each of the 290 plants analyzed. Note that large plants demonstrate relatively low CAPEX rates (green oval), while smaller plants demonstrate high CAPEX variability (red oval).

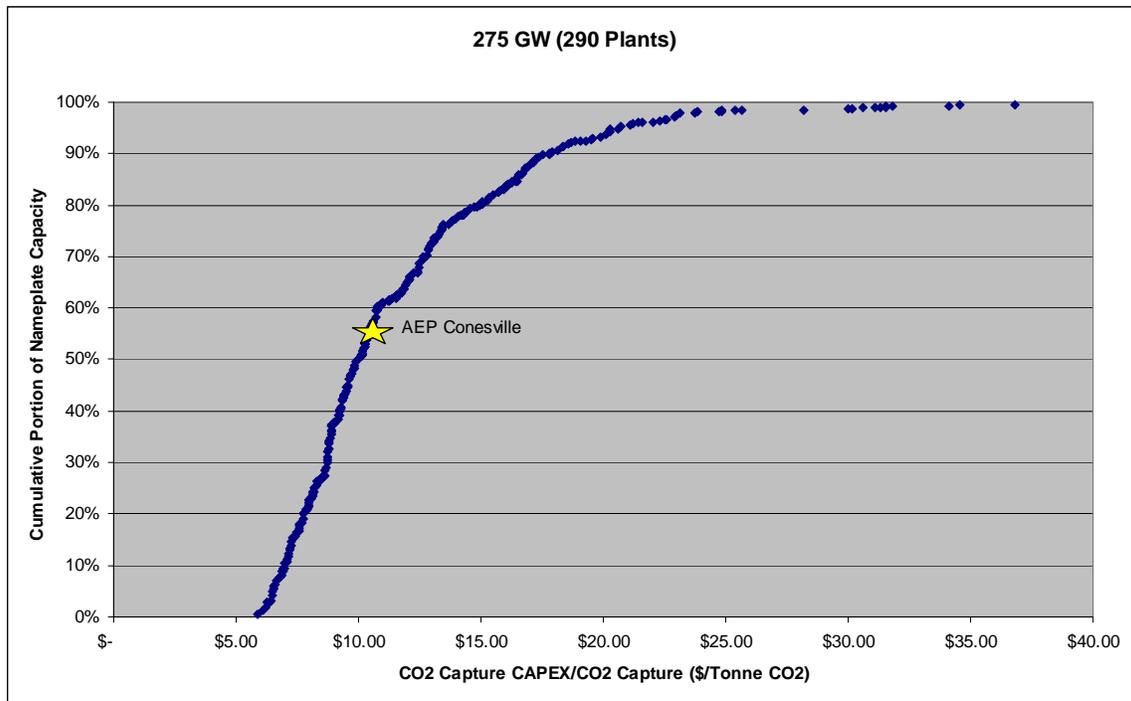


Figure 7. Cumulative nameplate capacity as a function of uncalibrated CO₂ capture CAPEX

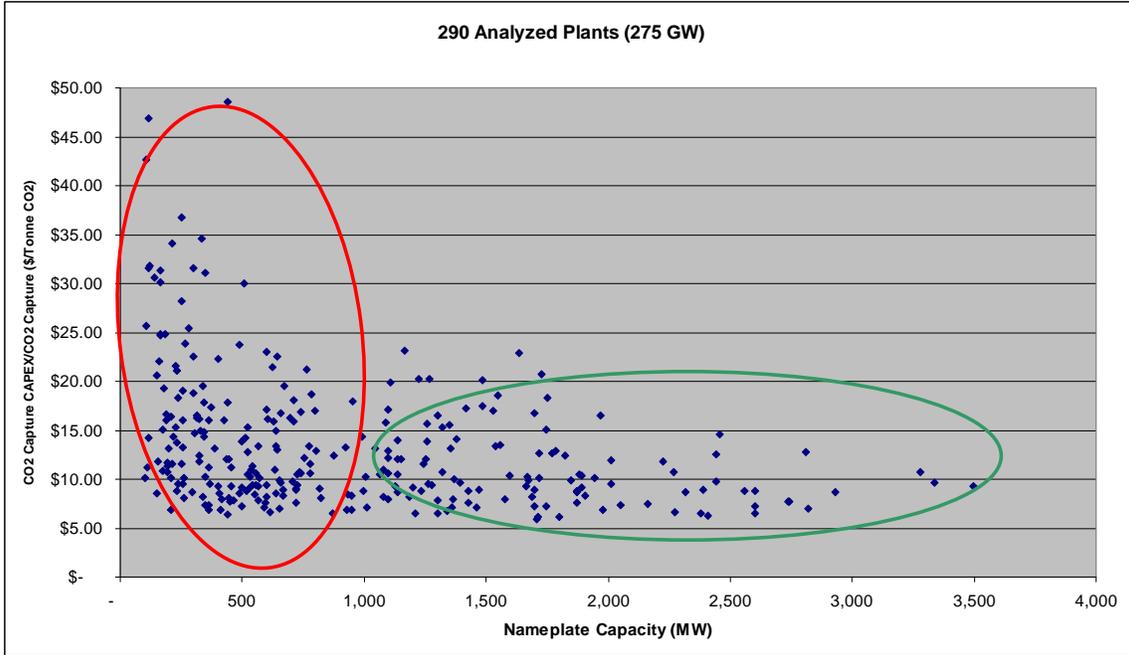


Figure 8. Nameplate capacity as a function of uncalibrated CO₂ capture CAPEX by plant

Figures 9 and 10 show cumulative nameplate capacity as functions of CO₂ OPEX and parasitic cost, respectively. Parasitic costs were calculated using a value for replacement electricity of \$0.05 per kWh.

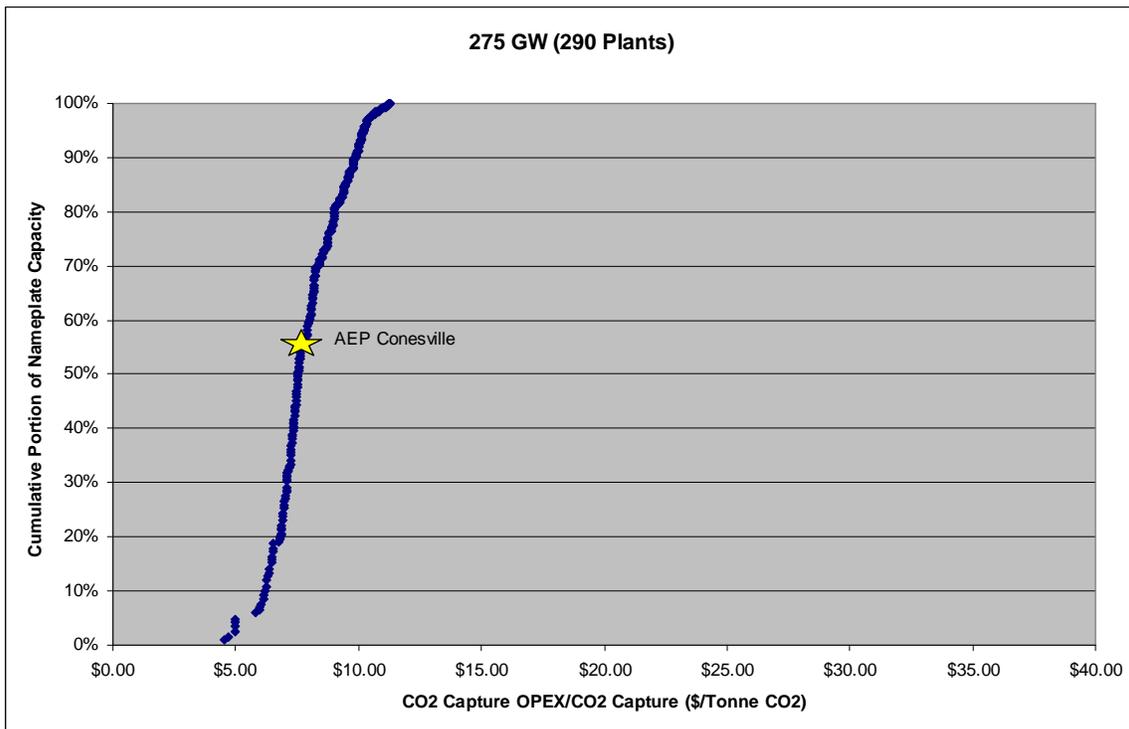


Figure 9. Cumulative nameplate capacity as a function of CO₂ capture OPEX

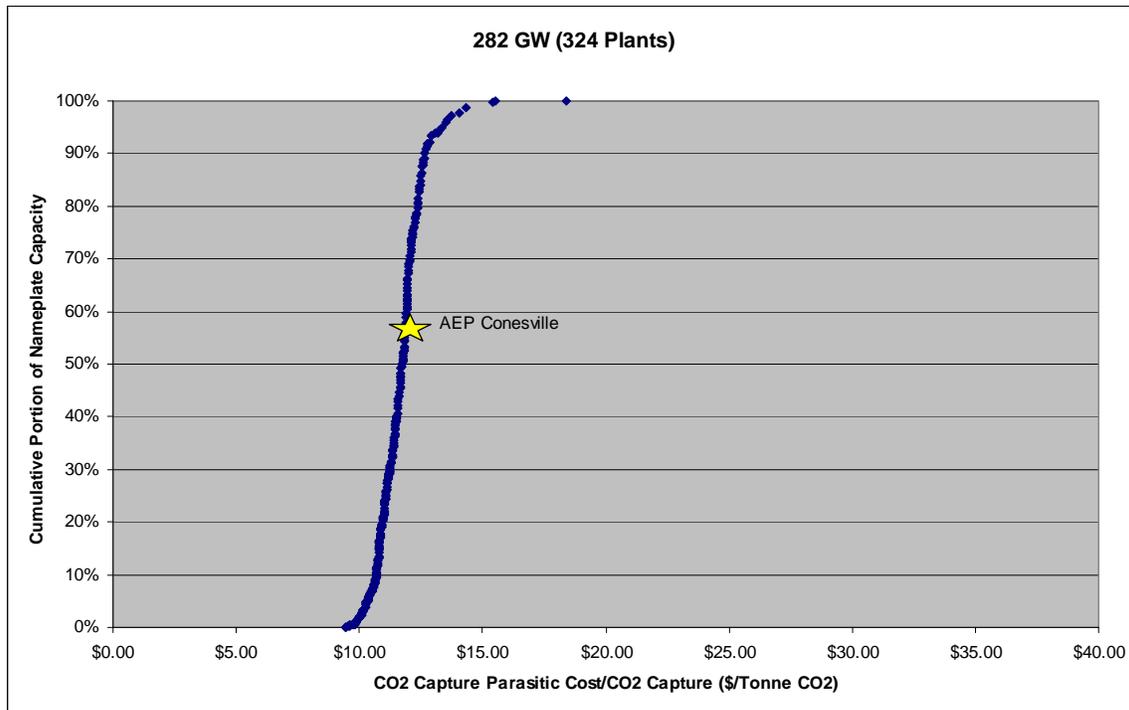


Figure 10. Cumulative nameplate capacity as a function of uncalibrated CO₂ capture parasitic cost

Figure 11 shows cumulative nameplate capacity as a function of uncalibrated total CO₂ capture cost. The CCM calculates total cost as the sum of CAPEX, OPEX, and parasitic cost. Cost of permitting and financing were not considered. For plants in the 50th percentile, the total CO₂ capture cost is less than \$29/tonne.

To calibrate the results derived in Figure 11 to full costs relative to the Conesville study, a comparison of the total costs from Unit 5 at Conesville was made relative to the results from the CCM. This ratio was used to scale the total costs (Figure 12). Results of the analysis indicate that, for the 50th percentile (142 GW) of the analyzed viable population, the calibrated CO₂ capture total cost would be about \$61/tonne or less. To retrofit 90 percent of generation capacity (about 254 GW), the total capture cost would be about \$80 per tonne or less. It should be noted that this study provides an overview of the plant sites. It is not an engineering-level analysis of individual plants and does not address the consequences of design.

Analysis of the study population shows that if all operating plants greater than 100 MW in size were to increase their efficiencies to achieve a heat rate of 12,500 Btu/kWh, an additional 85 GW could be suitable for CO₂ capture retrofits.

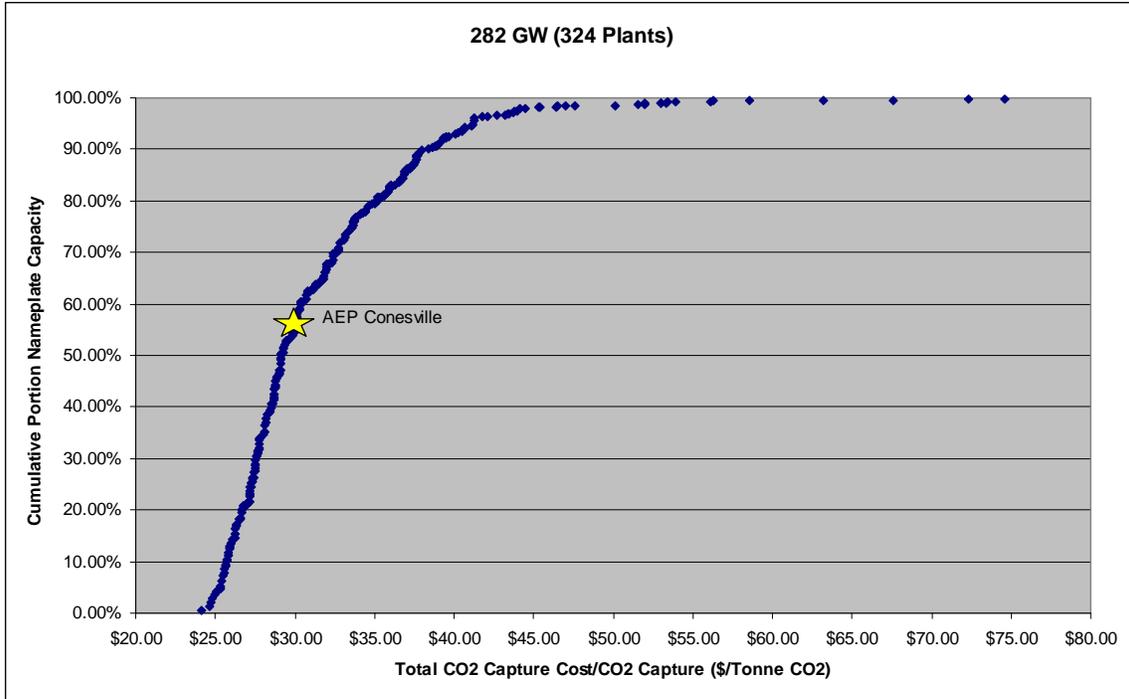


Figure 11. Cumulative nameplate capacity as a function of uncalibrated CO₂ capture total cost

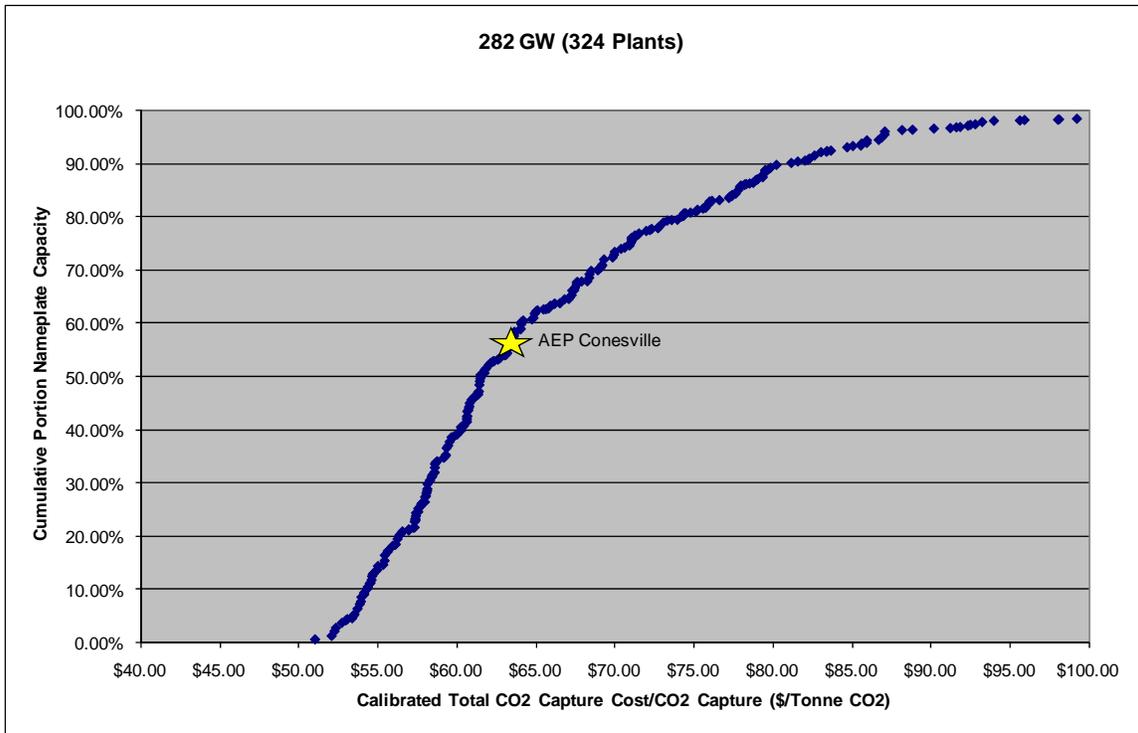


Figure 12. Cumulative nameplate capacity as a function of calibrated CO₂ capture total cost



Coal-fired Power Plants in the U.S.: Costs for Retrofit with CO₂ Capture Technology

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Rationale

- **Given the importance of coal to power generation in the United States, examination of the costs and practicability for retrofit of existing pulverized coal power plants with CO₂ capture technology is critical.**
- **This study defines a viable population of pulverized coal plants, where each plant was examined *discretely* to determine costs and space availability for retrofit.**
- **The effort was designed to enhance DOE's ability to analyze the opportunity for carbon capture retrofit of the nation's PC plant fleet for general equilibrium models.**

Overview

- **Base information (reports and datasets)**
- **Defining the viable population**
- **Model development and analysis**
- **Results**
 - CAPEX, OPEX, Parasitic costs
 - LCOE
 - CO₂ costs (captured and avoided)
- **Limitations**

Up-front Results

- Analyzed a population of 290 PC power plants for retrofit with carbon capture technology
- Analysis considers costs only associated with the retrofit (i.e., base plant CAPEX, OPEX *not* considered)
 - LCOE: median value of \$77/MW-h
 - Ranges from \$55/MW-h (10th percentile) to \$109 (90th percentile)
 - Carbon capture costs: median value of \$64/tonne
 - Ranges from \$54/tonne (10th percentile) to \$91 (90th percentile)
 - Carbon avoided costs: median value of \$91/tonne
 - Ranges from \$71/tonne (10th percentile) to \$130 (90th percentile)

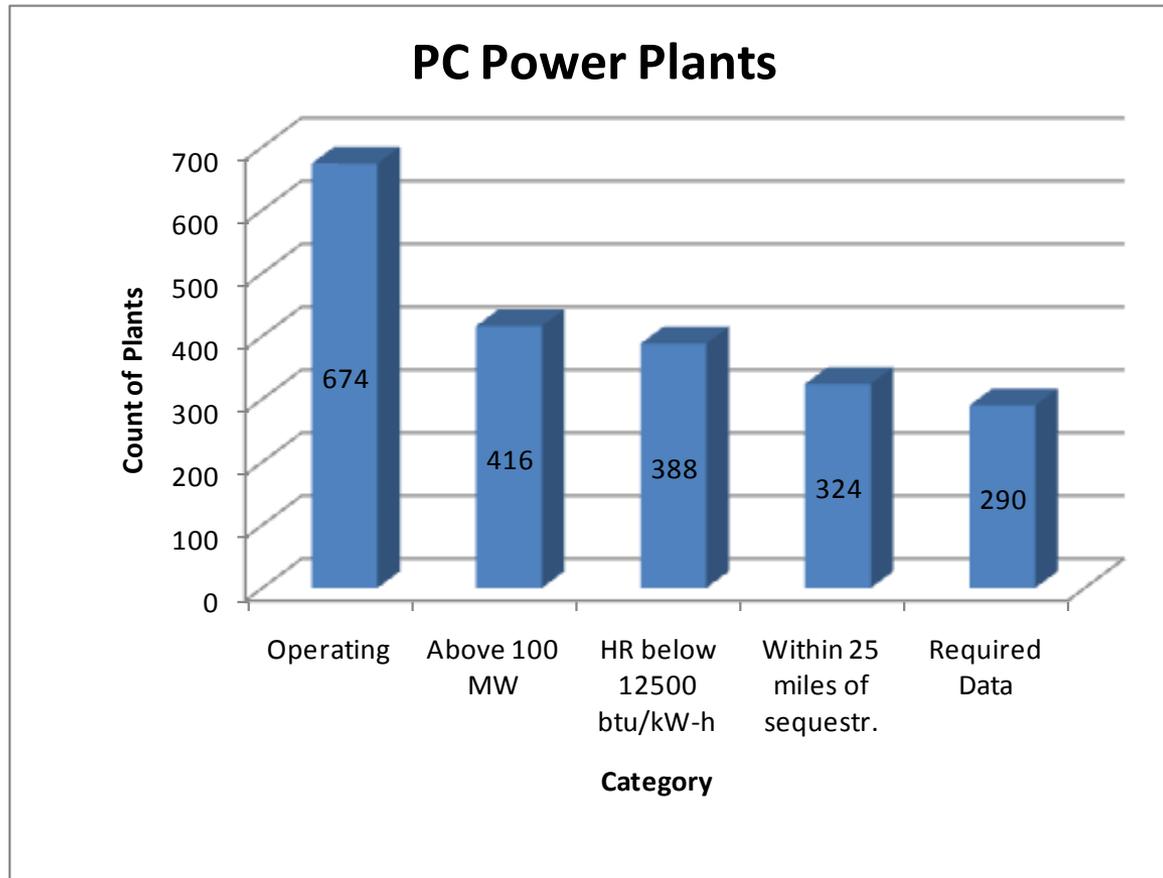
Information Sources

- **National Energy Technology Laboratory (“type” retrofit data (“Conesville Study”*), cooling water requirements)**
- **Energy Velocity Suite**
- **GIS data and image sources (e.g., Terraserver)**
- **U.S. Geological Survey (O&G production, water availability)**
- **NatCarb (saline aquifers, existing CO₂ pipelines)**
- **EIA (Electricity Market Modules)**

**AEP Conesville plant, subject of the report: DOE/NETL-2007/1281, Volume 1: Bituminous Coal and Natural Gas to Electricity, Final Report, Revision 1, August 2007*

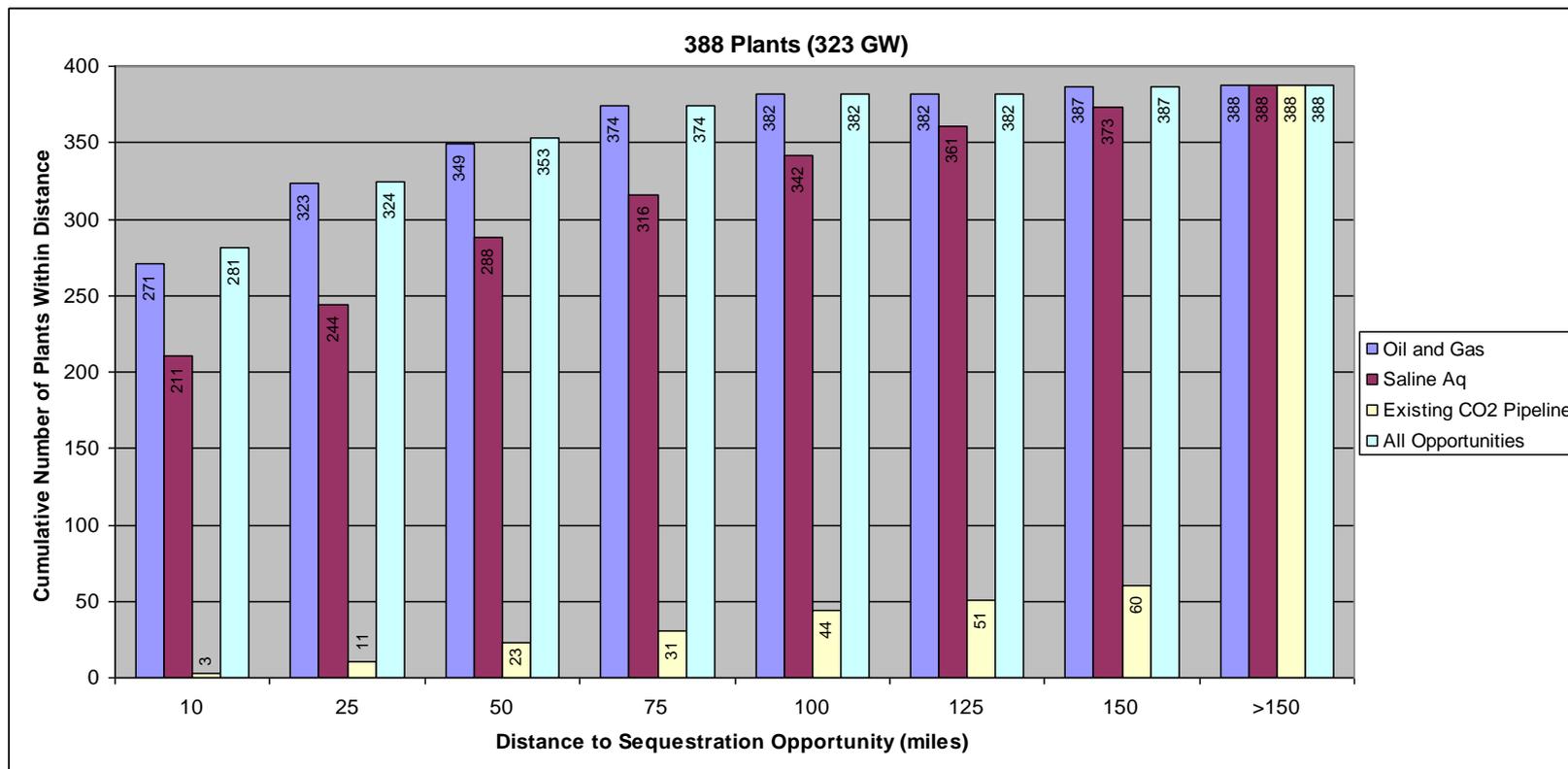
Defining the Viable Population

- The viable population was defined by size, heat rate and proximity to a sequestration opportunity



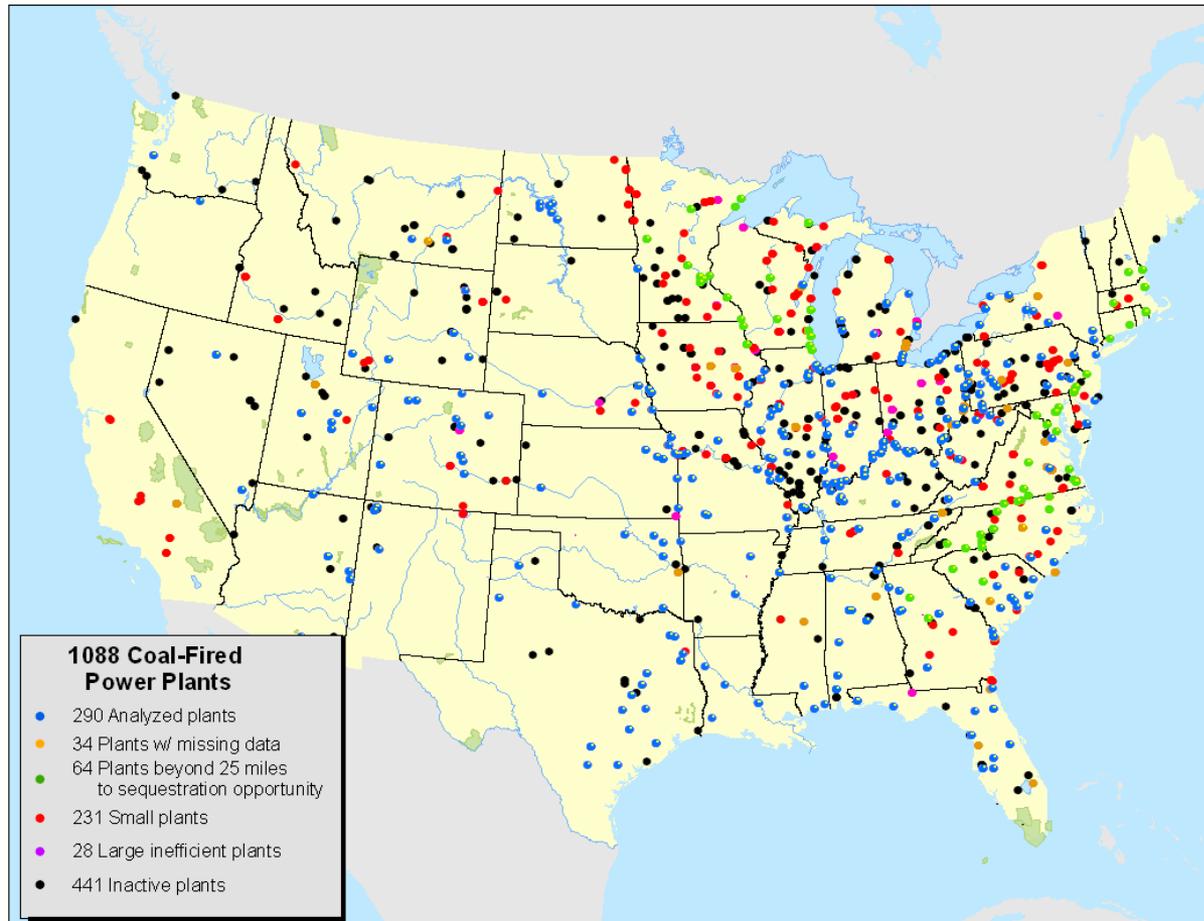
Defining the Viable Population (cont'd)

- Defining the distance to potential sequestration opportunities using an analytical GIS (geographic information system)—a 25 mile cutoff used



Defining the Viable Population (cont'd)

- **Viable Population of Coal-Fired Power Plants**

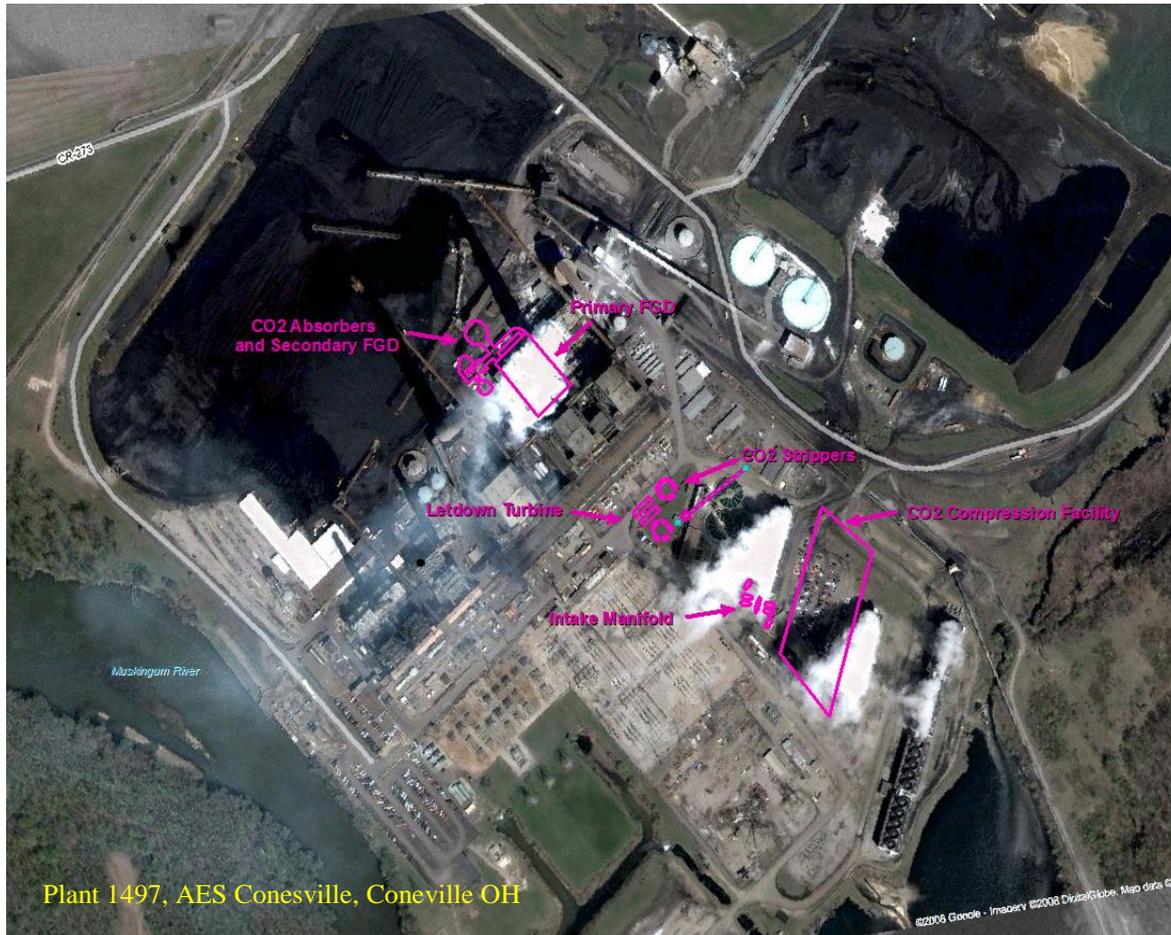


Model Development and Analysis

- **The Carbon Capture Model (CCM) was developed to read and analyze the various disparate datasets**
 - **Functions by reading parameters from the EV datasets and GIS data sources for each plant in the viable population**
 - **CCM calculates the required size and cost for the various CO₂ capture components using the Conesville study to determine scaling functionality**
 - **Costs are adjusted for construction difficulty, water availability, and additional land requirements**
 - **Assumptions:**
 - **A twenty-year future plant life**
 - **90 percent capture of carbon**

Model Development and Analysis (cont'd)

- Physical Size and Cost Scaling



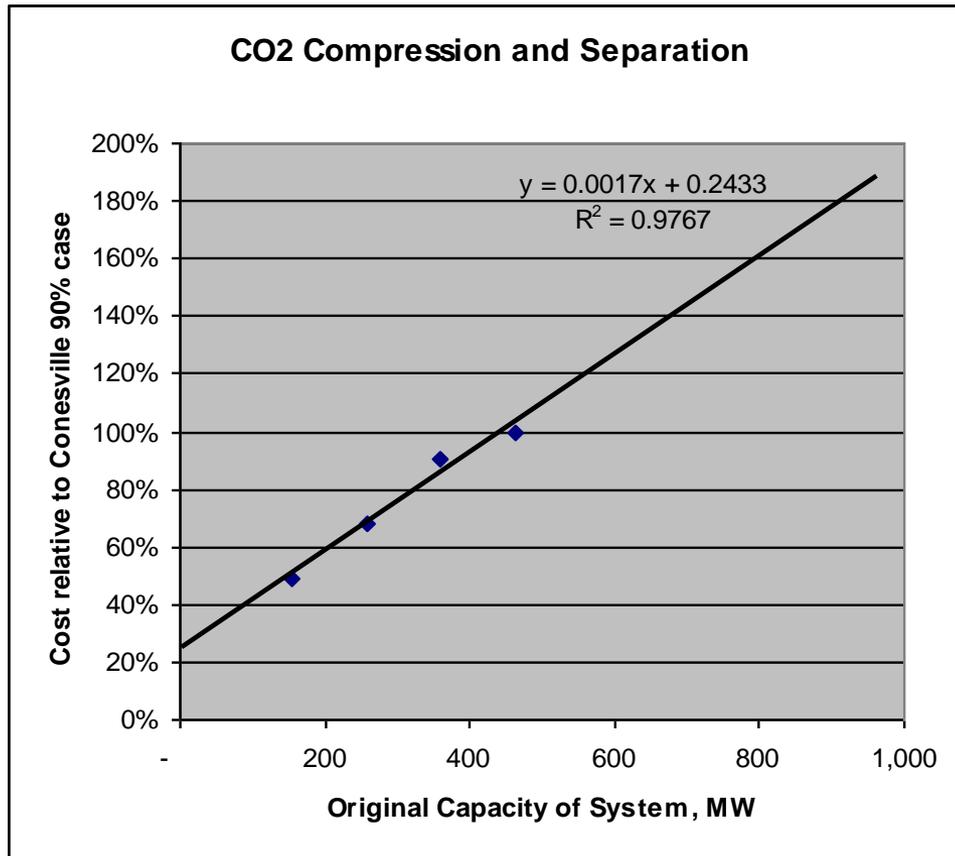
- Required equipment geometries were digitized from the Conesville Study so they could be scaled, relocated, and rotated to accommodate the remaining plants in the viable population

Model Development and Analysis (cont'd)

- **SO₂ Removal**
 - **SO₂ emissions required to be at or below 10 ppm for purposes of CO₂ capture so that the amine process can function properly**
 - **CCM determines the marginal SO₂ for removal on a volumetric (molar) basis relative to the CO₂ generated at each power plant**
 - **Calculation of the marginal SO₂ inherently incorporates primary FGD to the extent it exists at each unit**
 - **SO₂ removal “polishing” calculated discretely**
 - **CCM also estimates a plant’s overall SO₂ scrubbing efficiency**
- **NOx Removal**
 - **NOx emissions to be at or below 0.07 lbs NOx/ million Btu for purposes of CO₂ capture**
 - **Installation cost of \$300/tonne NOx used**

Model Development and Analysis (cont'd)

- CO₂ Compression and Separation Cost and Size Scaling



- Separation and compression handled individually.

Model Development and Analysis (cont'd)

- **Recirculating Cooling Cost and Size Scaling**
 - Assumed that a retrofitted unit would require 50 percent more recirculating cooling than an unretrofitted unit
 - Calculated using a unit's nameplate capacity and heat-rate to determine the heat generated per hour by a unit (as area/Btu/hr)



Current and additional recirculating cooling at the Conesville plant

Model Development and Analysis (cont'd)

- **Additional cost and/or physical size scaling provided for:**
 - **Let-down turbine**
 - **Discounting of incremental plant units**
 - **Additional land requirements**
 - **Water availability**

Model Development and Analysis (cont'd)

- **Construction Difficulty Factors**
 - In analyzing the sampled plant sites it becomes readily apparent that some plants are more crowded than others. Two incremental construction cost factors were developed to accommodate this situation:
 - **Close-in Construction**
 - The letdown turbine, separation equipment, CO₂ scrubbers and absorbers, as well as the primary and secondary FGDs require construction in close proximity to the main turbine and flue stack.
 - Ranged from 0 (easily constructed) to 40 percent (difficult to construct) based on the examination of the GIS

Model Development and Analysis (cont'd)

- **Construction Difficulty Factors (cont'd)**
 - **Landscape Construction**
 - Addresses CO₂ compression and additional cooling facilities
 - Ranges from 0-30 percent
 - **Construction factors applied incrementally, where**
 - **Cost = Conesville costs_{scaled} * (1+ Construction Difficulty Factor)**
 - **Overall, an estimated 8 to 10 additional acres are required for the retrofit technology footprint at the average site**

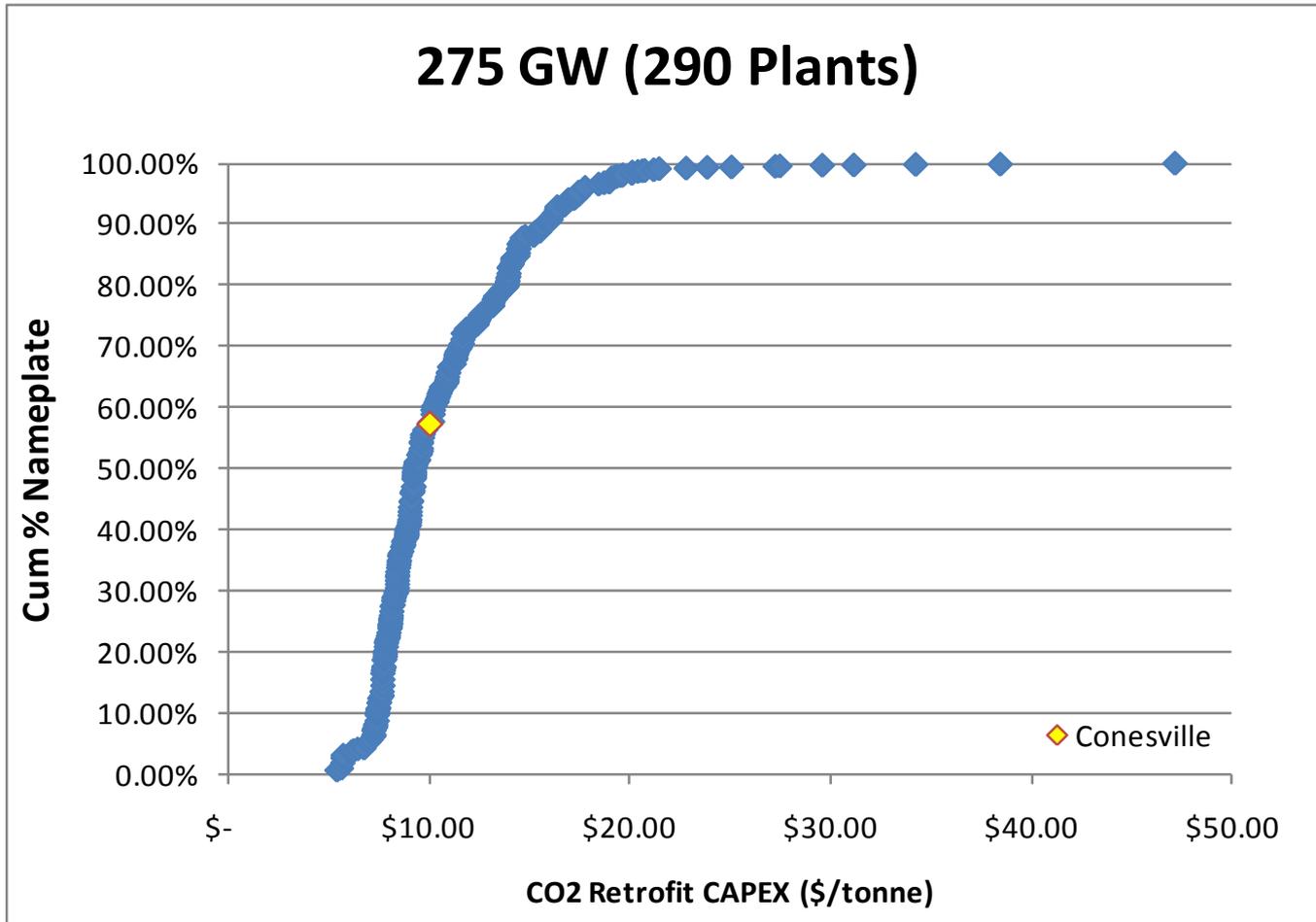
Model Development and Analysis (cont'd)

- **Investment CAPEX**—sum of capital items
- **OPEX**—calculated as the sum of
 - Fixed, variable, feedstock
- **Parasitic Load**
 - Computed as the sum of the parasitic loads of newly installed NO_x and SO₂ control equipment, additional cooling, and the CO₂ retrofit components
- **LCOE**
 - 20-year levelization; make-up power priced at \$0.05/kW-h
- **CO₂ costs**
 - Capture
 - Avoided (based on snapshot of conditions in EMMs)

RESULTS

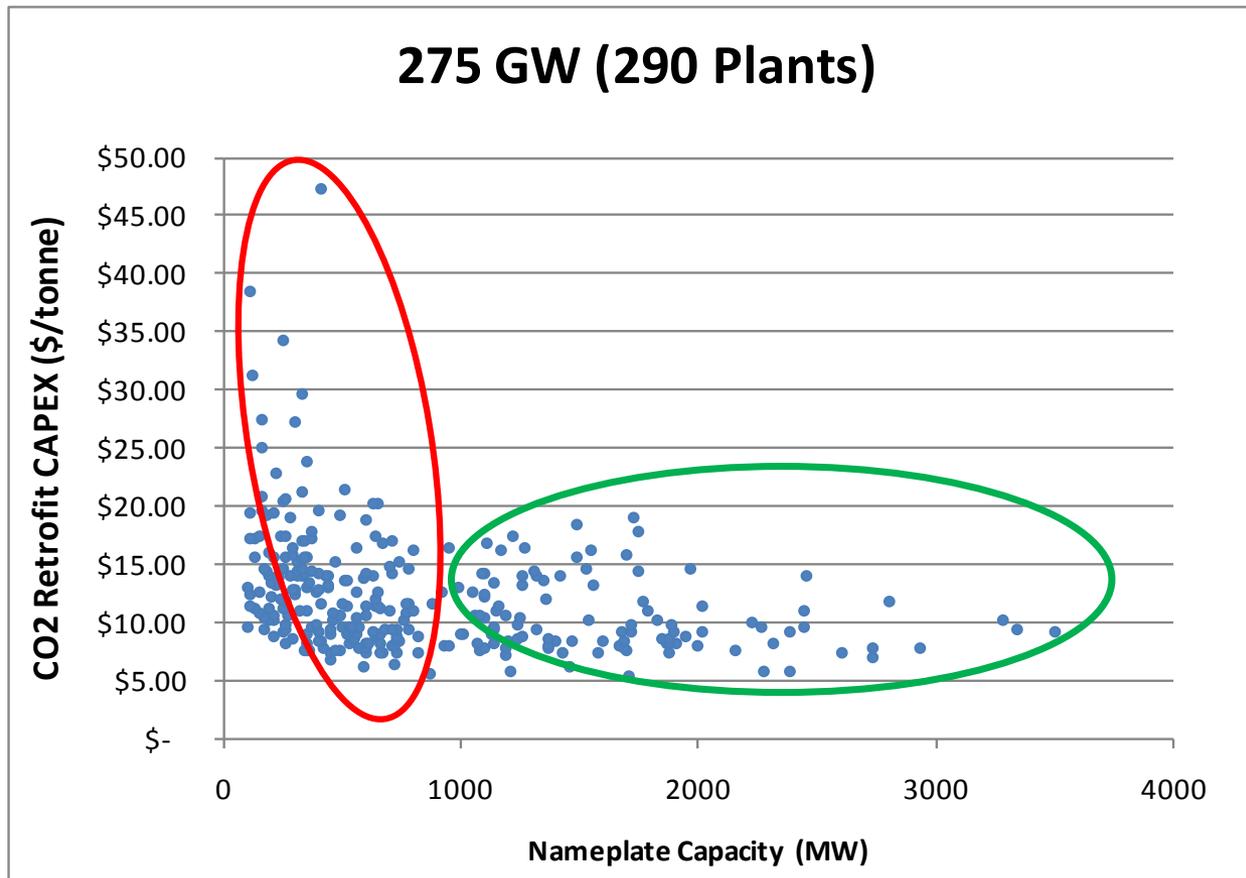
Analytical Results

- CAPEX investment cost as a function of nameplate capacity



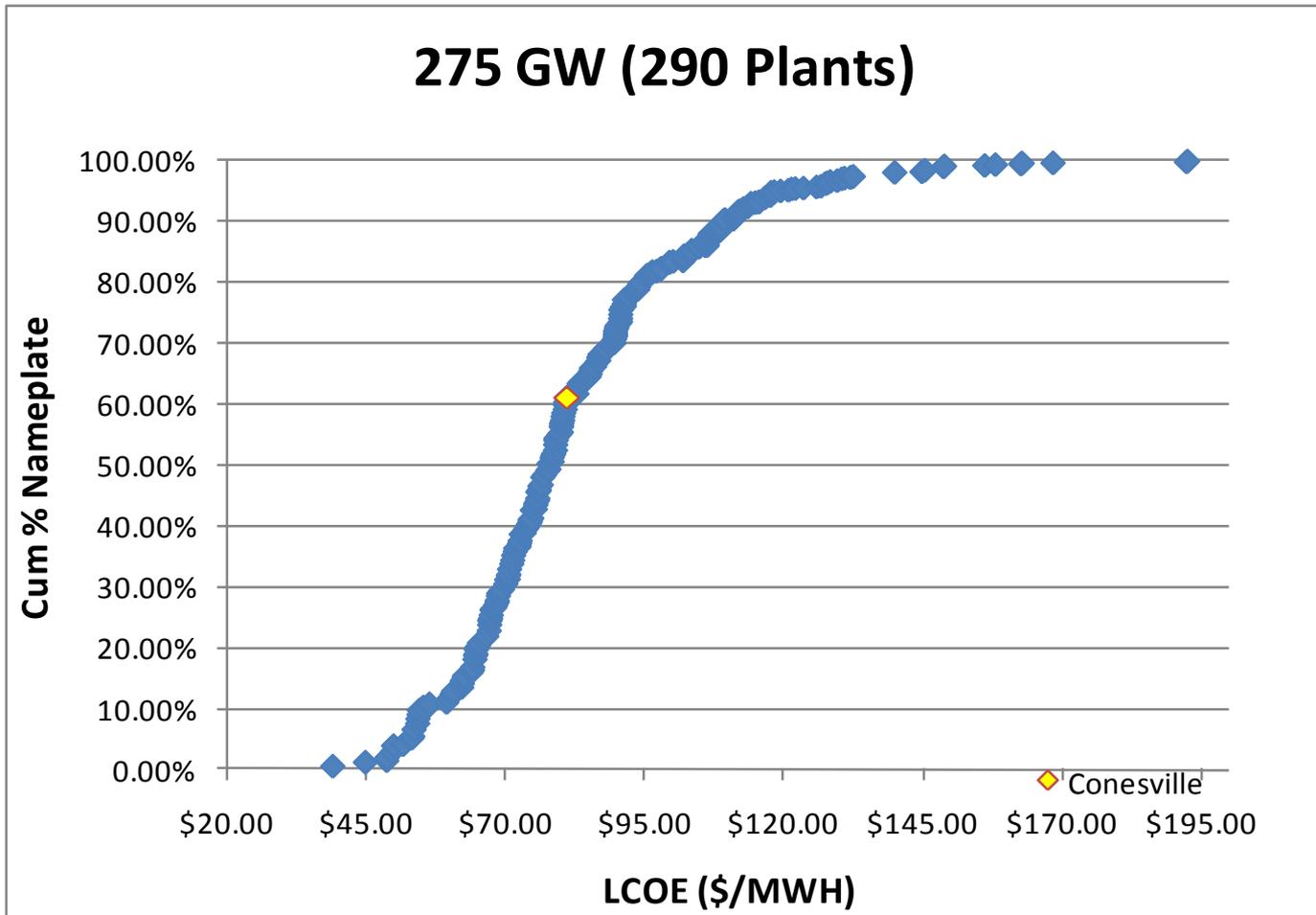
Analytical Results (cont'd)

- The majority of large plants demonstrate relatively low uncalibrated CAPEX rates, while smaller plants demonstrate high CAPEX variability



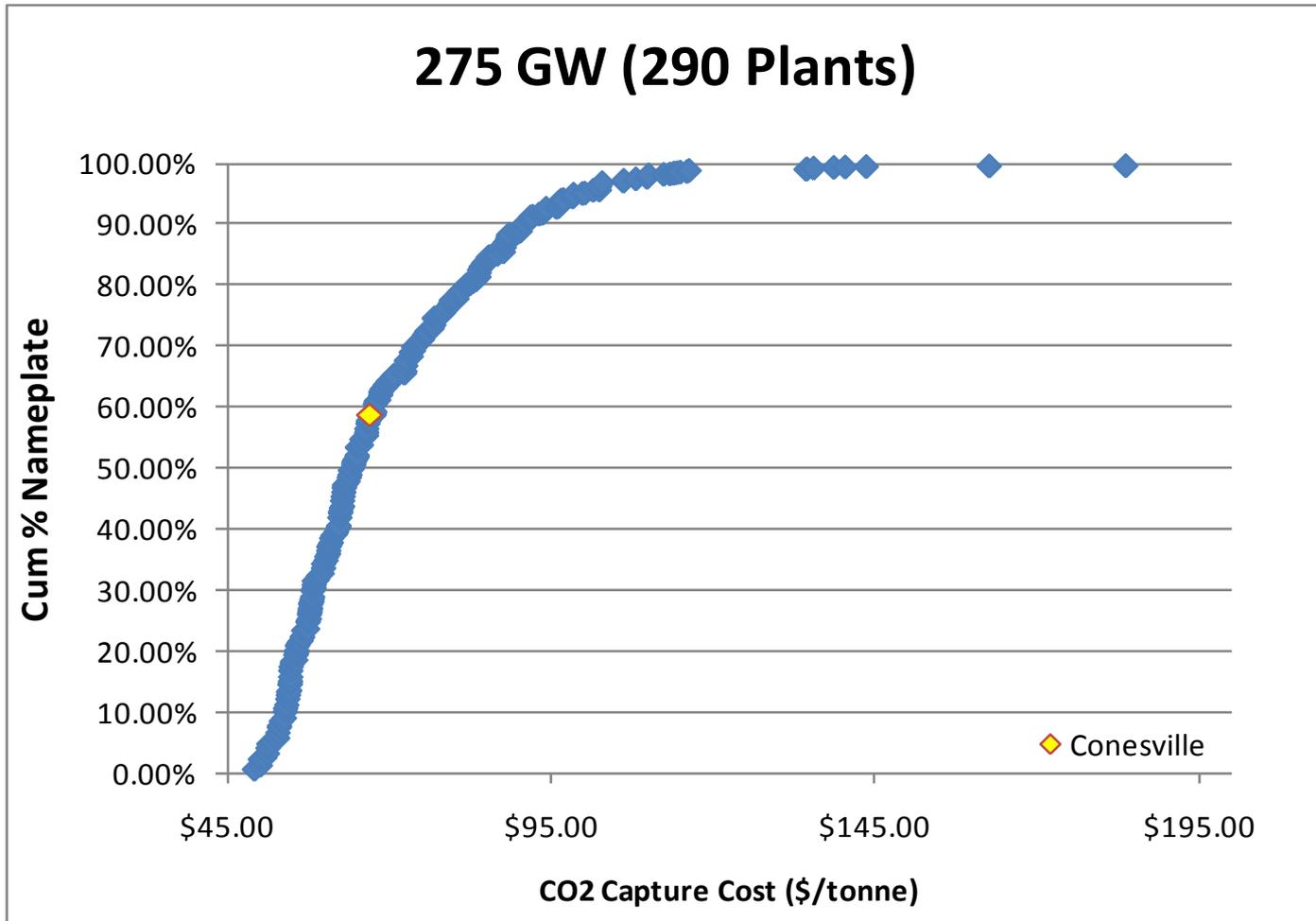
Analytical Results (cont'd)

- LCOE for the retrofits (based on \$0.05/kW-h make-up cost)



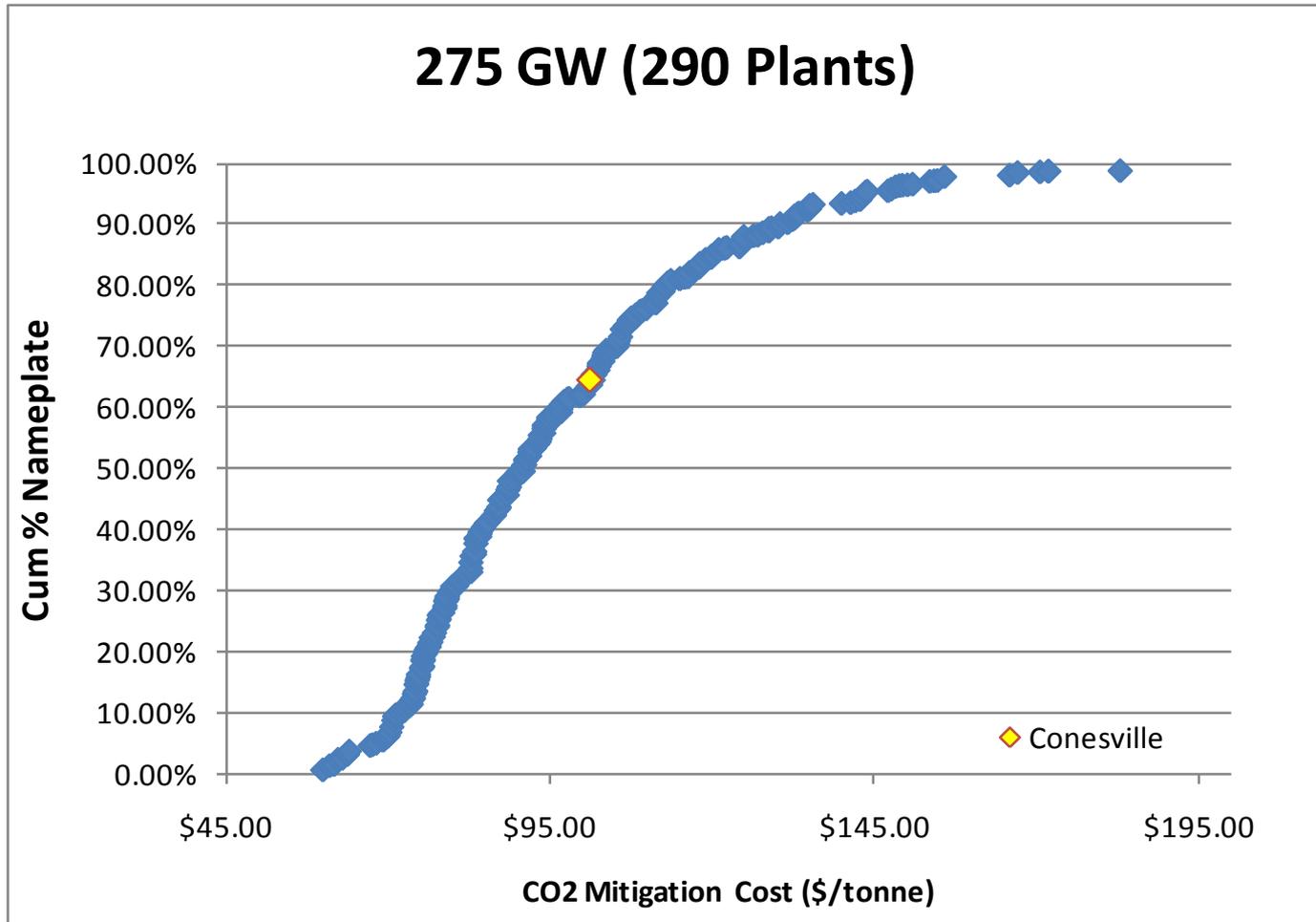
Analytical Results (cont'd)

- CO₂ capture cost



Analytical Results (cont'd)

- **Avoided CO₂ cost**



Limitations

- **Study is indicative of cost structure of the analyzed population relative to the Conesville Study**
- **Study is not an engineering-level analysis of individual plants; it does not address the consequences of design**

Acknowledgments

This work was funded by the U.S. Department of Energy's National Energy Technology Laboratory (U.S. DOE/NETL). The NETL sponsor for this project, Philip DiPietro, Director of the Situational Analysis and Benefits Division, Office of Systems, Analyses and Planning (OSAP), provided guidance and technical oversight for this study. The authors gratefully acknowledge the significant role played by U.S. DOE/NETL in providing the programmatic guidance and review of this study.

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